



(11) **EP 1 118 370 A1**

(12) **EUROPEAN PATENT APPLICATION**

(43) Date of publication:
25.07.2001 Bulletin 2001/30

(51) Int Cl.7: **B01D 53/047, C01B 3/02**

(21) Application number: **01100128.6**

(22) Date of filing: **15.01.2001**

(84) Designated Contracting States:
AT BE CH CY DE DK ES FI FR GB GR IE IT LI LU
MC NL PT SE TR
 Designated Extension States:
AL LT LV MK RO SI

- Weist, Edward Landis Jr.
 Macungie, PA 18062 (US)
- Rarig, David Lester
 Emmaus, PA 18049 (US)
- Occhialini, James Michael
 New Tripoli, PA 18066 (US)
- Pillarella, Mark Robert
 Center Valley, PA 18034 (US)

(30) Priority: **20.01.2000 US 488648**

(71) Applicant: **AIR PRODUCTS AND CHEMICALS, INC.**
Allentown, PA 18195-1501 (US)

(74) Representative: **Schwabe - Sandmair - Marx**
Stuntzstrasse 16
81677 München (DE)

(72) Inventors:
 • Xu, JIanguo
Wrightstown, PA 18940 (US)

(54) **Pressure swing adsorption process with multiple adsorption beds**

(57) A pressure swing adsorption process includes providing an adsorption apparatus having a plurality of beds and counter-currently purging at least two of the beds simultaneously throughout the process. The number of beds and number of pressure equalization steps are not particularly limited, but a ten-bed, four pressure equalization step process is advantageous. In

addition, other ten-bed, four pressure equalization step processes are disclosed which do not counter-currently purge at least two of the beds simultaneously, but which have an average of at least two of the ten beds being simultaneously regenerated by simultaneously providing off-gas from a feed end of each of the two beds to an off-gas line.

EP 1 118 370 A1

EP 1 118 370 A1

Description

CROSS-REFERENCE TO RELATED APPLICATIONS

5 [0001] Not applicable.

BACKGROUND OF THE INVENTION

10 [0002] This invention relates to pressure swing adsorption (PSA) processes, and more particularly to such processes employing multiple adsorbent beds and multiple pressure equalization steps.

[0003] PSA processes are well-known for the separation of gas mixtures that contain components with different adsorbing characteristics. For example, hydrogen production via pressure swing adsorption (H_2 PSA) is a multi-million dollar industry supplying high purity hydrogen for chemical producing industries, metals refining and other related industries.

15 [0004] In a typical PSA system, a multicomponent gas is passed to at least one of multiple adsorption beds at an elevated pressure to adsorb at least one strongly sorbed component while at least one component passes through. In the case of H_2 PSA, H_2 is the most weakly adsorbed component which passes through the bed. At a defined time, the feed step is discontinued and the adsorption bed is depressurized with flow co-current to the direction of the feed in one or more steps which permits essentially pure H_2 product to exit the bed with a high recovery of the most weakly adsorbed component, H_2 . Then a countercurrent desorption step is carried out, followed by countercurrent purge and repressurization.

20 [0005] U.S. Patent No. 3,986,849 to Fuderer et al. discloses PSA processes employing at least seven adsorbent beds, at least three steps of pressure equalization per bed. This patent teaches that an undesirable reversion of the desorbate profile from the inlet to the discharge end of the bed is substantially reduced when at least three pressure equalization stages are employed. Fuderer et al. does not disclose any embodiments comprising performing four pressure equalization steps in a ten-bed apparatus, or process cycles with on average two or more beds being purged at the same time.

25 [0006] The prior art in general teaches that increasing the number of beds typically facilitates increasing the number of equalizations, which minimizes the production costs of a PSA system. Unfortunately, increasing the number of beds typically increases the cost of a PSA system as well.

[0007] Accordingly, it would be very desirable to provide an improved PSA process which increases production and/or recovery per bed in a multiple bed system.

[0008] All references cited herein are incorporated herein by reference in their entireties.

35 BRIEF SUMMARY OF THE INVENTION

[0009] The invention provides a pressure swing adsorption process comprising providing a pressure swing adsorption apparatus having ten beds, and equalizing a pressure of each of said ten beds in four steps. At all times during the process, an average of at least two of said ten beds are being simultaneously regenerated by simultaneously providing off-gas from a product end of each of said two beds to an offgas line. Each of the four pressure equalization steps comprises a depressurization phase spanning about 1/20 of a total cycle time of said process and a repressurization phase spanning about 1/20 of said total cycle time. The preferred product of the process is hydrogen.

40 [0010] The invention also provides a pressure swing adsorption process in which an average of at least two beds are being counter-currently purged throughout the process cycle.

45

BRIEF DESCRIPTION OF SEVERAL VIEWS OF THE DRAWINGS

Not applicable.

50 DETAILED DESCRIPTION OF THE INVENTION

[0011] In a first embodiment of the invention, the improved PSA system employs ten adsorbent beds and four steps of equalization. Preferably, an average of at least two of said ten beds are simultaneously regenerated by simultaneously providing off-gas from a feed end of each of said two beds to an off-gas line throughout said process. Preferably, each of said four steps comprises a depressurizing provide equalization phase spanning about 1/20 of a total cycle time of said process and a repressurization phase "R" spanning about 1/20 of said total cycle time. The preferred product of the invention is hydrogen.

55 [0012] A second embodiment of the invention is based on the inventors' discovery that the average bed pressure

EP 1 118 370 A1

during the purge step is very important in determining the recovery and productivity of the adsorption system. It is desirable to use a longer purge time to reduce the pressure drop in the bed, and therefore reduce the average bed pressure during the purge step. The slower the purge rates, the more effective a system is in removing adsorbed gases. Thus, the second embodiment of the invention requires that, at all times throughout the process, at least two beds are being counter-currently purged at the same time.

[0013] In a preferred embodiment, the process comprises:

- (a) at least one adsorption step comprising feeding a feed mixture to a feed end of a first bed, adsorbing impurities onto an adsorbent in said first bed and permitting a product gas to exit a product end of said first bed;
- (b) at least one depressurizing equalization step comprising reducing a pressure in said first bed by closing a feed valve and sequentially releasing gas from a product end of said first bed to other beds or to at least one other bed and a tank;
- (c) at least one pressure reduction step comprising further reducing said pressure of said first bed co-currently and/or counter-currently;
- (d) at least one counter-current purging step, comprising counter-currently purging said first bed with gas from another bed for a duration such that at least two of said beds of said apparatus are being purged simultaneously throughout said process;
- (e) at least one repressurizing equalization step comprising increasing the pressure of said first bed with gas released from at least one other bed and/or tank undergoing said pressure reducing step; and
- (f) at least one pressure augmentation step comprising further increasing said pressure of said first bed by feeding to said first bed at least one of a counter-current stream of product gas and a co-current stream of feed gas. In certain embodiments, steps (a) to (f) are sequential.

[0014] The preferred product gas is hydrogen, but the invention is not limited thereto.

[0015] Preferably, the feed mixture comprises hydrogen and at least one member selected from the group consisting of methane, carbon dioxide, carbon monoxide, nitrogen and water vapor.

[0016] In embodiments, the feed gas is obtained by steam reforming of hydrocarbons.

[0017] In other embodiments, the feed gas is obtained by partial oxidation of hydrocarbons. In a number of these embodiments, the partial oxidation can occur in the presence of at least one catalyst.

[0018] In embodiments wherein the oxygen used for oxidation is provided by an ion transport membrane, it is preferred that the ion transport membrane be integrated with a reactor in which the partial oxidation occurs.

[0019] In embodiments, at least a part of said at least one repressurizing equalization step overlaps in time with said at least one pressure augmentation step.

[0020] In embodiments, at least a part of said at least one repressurizing equalization step overlaps in time with at least one of counter-current repressurization by the product gas and co-current repressurization by the feed gas.

[0021] In embodiments, gas from the product end of the bed in said at least one depressurizing equalization step is transferred directly to a bed in said at least one repressurizing equalization step.

[0022] In embodiments, gas from the product end of the bed in said at least one depressurizing equalization step is transferred to a tank before being transferred to a bed in said at least one repressurizing equalization step.

[0023] In embodiments, a bed being co-currently depressurized according to said at least one pressure reduction step provides purge gas to more than one other bed.

[0024] In embodiments, the depressurizing equalization step precedes said provide purge step, in other embodiments, the depressurizing equalization step overlaps in time with at least some portion of said provide purge step, and in still other embodiments, the depressurizing equalization step follows said provide purge step.

[0025] In embodiments, a bed being co-currently depressurized according to said at least one pressure reduction step provides gas for pressure equalization of at least one other bed, as well as purge gas to more than one other bed.

[0026] In embodiments, the bed at step (c) has at least one counter-current depressurization step.

[0027] In embodiments, the counter-current depressurization step immediately precedes the counter-current purge step (d).

[0028] The invention is most efficiently described through the use of cycle charts, which are readily understood by those of ordinary skill in the art. In the cycle charts shown herein, each column represents a time period of the cycle and each row represents a bed. The following table shows the cycle chart of a process that is presented for purposes of comparison only.

4

EP 1 118 370 A1

[0029] In the first step of this cycle for the first bed, the feed goes to a bed from the feed end for 1/3 of the cycle time to produce hydrogen from the product end in the first step. During this period, the pressurized feed flows through the bed. The impurities in the feed, such as CO₂, methane, CO and nitrogen, are adsorbed by the adsorbents. Hydrogen, on the other hand, is less strongly adsorbed and is driven out of the bed as hydrogen product. This step is called the "adsorption" step and is indicated by "A's" in Table 1.

[0030] In the second step, feed to the first bed is stopped. The hydrogen from the product end of this bed (the first bed) is now fed to the product end of another bed (the second bed) whose pressure is being increased. That process goes on for approximately 1/24 of the cycle time, until the pressures in these two beds are almost equal. This step is indicated by "1" in the cycle chart, standing for the depressurization phase of pressure equalization step one.

[0031] In the third step, the product end of the first bed is disconnected from the second bed and connected to the product end of the third bed whose pressure is lower than the first and second beds. This goes on for approximately 1/24 of the cycle time, until the pressures in these two beds are close to each other. This step is indicated by "2" in the cycle chart, meaning that this is the depressurization phase of pressure equalization step two.

[0032] In the fourth step, the connection between these two beds is then cut off, and hydrogen from the product end of the first bed is fed to the product end of the fourth bed, whose pressure is yet lower than the third bed at the beginning of the previous step. This process again goes on for approximately 1/24 of the cycle time until the pressures of the two beds are close to each other. This step is indicated by "3" in the cycle chart, standing for the depressurization phase of pressure equalization step three.

[0033] In the fifth step, the connection between the first bed and the fourth bed is closed, and the hydrogen from the product end of the first bed is introduced into the fifth bed whose pressure is lower than that of the fourth bed at the beginning of the previous step, and which has just finished the "purge" step (step 8) and idle step (step 9). This process again lasts for 1/24 of the cycle time, and at the end of this step, the pressures in these two beds are again close to each other. This step is indicated by "4" in the cycle chart, representing the depressurization phase of pressure equalization step four.

[0034] In the sixth step, the connection between the first bed and the fifth bed is closed, and the gas from the product end of the first bed is introduced to the product end of the sixth bed. The feed end of the bed being purged (the sixth bed) is connected to the offgas line and the gas purged from this bed enters the offgas line. This step lasts for approximately 1/12 of the cycle time, and is called the "provide purge" step, indicated by "P's" in the cycle chart.

[0035] In the seventh step, the product end valve is closed and the feed end is connected to the offgas line. The gas in the bed goes to the offgas line. This step lasts for 1/12 of the cycle time and is called the "countercurrent blowdown" step and is indicated by "B's" in the chart.

[0036] In the eighth step, the product end of the bed is connected to the product end of a bed in its sixth step (the "provide purge" step). The gas from the "provide purge" bed purges the bed and the impurities and some hydrogen gas leave this first bed (the bed being purged) from the feed end and enters the offgas line. This step lasts about for 1/12 of the cycle time and is called the "countercurrent purge" step. It is indicated by "G's" in the cycle chart.

[0037] In the ninth step, the bed is closed on both ends for 1/24 of the cycle time and this step is called the "idle" step, indicated by "I" in the cycle chart.

[0038] In the tenth step, the product end of the bed is connected to the product end of a bed at its fifth step. Gas flows from the product end of the bed at its fifth step and enters this bed from its product end. This takes about 1/24 of the cycle time until the pressures in the two beds are close to each other. This step is indicated by "4", indicating that it is at the receiving gas end of the fourth pressure equalization step following the sequence order of the pressure equalization steps. That is, "4" indicates the repressurization phase of the fourth pressure equalization step.

[0039] In the eleventh step, the product end of the bed is connected to the bed at the fourth step. Gas flows from the product end of the bed at its fourth step and enters this bed from its product end. This takes about 1/24 of the cycle time until the pressures in the two beds are close to each other. This step is indicated by "3", indicating that it is at the receiving gas end of third pressure equalization step. That is, "3" indicates the repressurization phase of the third pressure equalization step.

[0040] In the twelfth step, the product end of the bed is connected to the bed at the third step. Gas flows from the product end of the bed at its third step and enters this bed from its product end. This takes about 1/24 of the cycle time until the pressures in the two beds are close to each other. This step is indicated by "2", indicating that it is at the receiving gas end of the second pressure equalization step. That is, "2" indicates the repressurization phase of the second pressure equalization step.

[0041] In the thirteenth step, the product end of the bed is connected to the bed at the second step. Gas flows from the product end of the bed at its second step and enters this bed from its product end. This takes about 1/24 of the cycle time until the pressures in the two beds are close to each other. Some product gas also enters the product end of this bed. This step is indicated by "1", indicating that it is at the receiving gas end of the first pressure equalization step. That is, "1" indicates the repressurization phase of the first pressure equalization step.

[0042] Then in the fourteenth step, the connection between these two beds is closed while the gas from the product

EP 1 118 370 A1

line continues to re-pressurize the bed until the pressure in the bed is close to that of the product hydrogen. This step takes approximately 1/24 of the cycle time and is indicated by the letter "R" in the chart for "repressurization." After this step is finished, the bed returns to step 1.

[0043] The cycles of the twelve beds of Table 1 are staggered such that one bed starts adsorption 1/12 of the cycle time later than the previous one. Such a cycle has four beds generating products all the time. The time for pressure equalization does not have to be exactly $1/(2 \times n)$, in which "n" is the number of beds in the system. When the time for the first step of pressure equalization, "1", is "t" less than $1/(2 \times n)$ of the cycle time, the time for the receiving pressure equalization step, 1', is decreased by the same amount, while the time for re-pressurization step "R" is increased by the same amount. The time for the second pressure equalization step on both providing gas end and receiving gas end, 2 and 2', can be increased by the same amount. If the first and second equalization share a common valve/line arrangement and the third and fourth equalization share a common valve/line arrangement, the time for the third pressure equalization step on both providing gas end and receiving gas end, 3 and 3', must be reduced by at least t. The time for the fourth pressure equalization step on both providing gas end and receiving gas end, 4 and 4', can be increased by the same amount. The time for the idle can be decreased by the same amount. The same holds true for all the cycles discussed below (the idle step and the step solely consisting of providing gas for the lowest pressure equalization step, 4, do not exist for all the cycles).

[0044] The following table shows the cycle chart of a ten-bed cycle of the first embodiment of the invention with only two beds on adsorption:

TABLE 2

A	A	A	A	1	2	3	4	P	P	B	B	G	G	I	4'	3'	2'	1'	R
1'	R	A	A	A	A	1	2	3	4	P	P	B	B	G	G	I	4'	3'	2'
3'	2'	1'	R	A	A	A	A	1	2	3	4	P	P	B	B	G	G	I	4'
I	4'	3'	2'	1'	R	A	A	A	A	1	2	3	4	P	P	B	B	G	G
G	G	I	4'	3'	2'	1'	R	A	A	A	A	1	2	3	4	P	P	B	B
B	B	G	G	I	4'	3'	2'	1'	R	A	A	A	A	1	2	3	4	P	P
P	P	B	B	G	G	I	4'	3'	2'	1'	R	A	A	A	A	1	2	3	4
3	4	P	P	B	B	G	G	I	4'	3'	2'	1'	R	A	A	A	A	1	2
1	2	3	4	P	P	B	B	G	G	I	4'	3'	2'	1'	R	A	A	A	A
A	A	1	2	3	4	P	P	B	B	G	G	I	4'	3'	2'	1'	R	A	A

[0045] In this cycle, the bed is on adsorption for 1/5 of the cycle time. It then provides gas from the product end of the bed in the first, second, third, and fourth steps of pressure equalization sequentially, with each step lasting approximately 1/20 of the cycle time. The bed then provides gas for purge, again from the product end of the bed, for approximately 1/10 of the cycle time. Then the product end of the bed is closed and the feed end valve to the offgas line is opened. The gas in the bed is sent to the offgas line for approximately 1/10 of the cycle time, until the pressure in the bed is not much greater than that in the offgas line. Then the product end of the bed is connected to the product end of a bed that is at its "provide purge" step. This mostly hydrogen gas flows from the bed at its "provide purge" step to the bed under description, driving out some of the impurities in the bed to the offgas line. This lasts for approximately 1/10 of the cycle time. Then the bed sits idle for approximately 1/20 of the cycle time. It then receives gas from the product end of the bed in the steps of receiving pressure equalization, indicated by 4', 3', 2', and 1' in the cycle chart (i.e., Table 1), with each step lasting for approximately 1/20 of the cycle time, until the pressure of the bed is close to that in the bed providing gas for pressure equalization in each step. In the last of these receiving pressure equalization gas steps, some product gas is also fed to the product end of the bed. Then, in the last step, the connection of this bed with the provide equalization gas bed is cut and the product gas continues to enter the bed from the product end for approximately 1/20 of the cycle time until the pressure of the bed is close to that of the product. This bed thereby completes one cycle and returns to the adsorption step. The ten beds are staggered by starting the cycle of the subsequent bed 1/10 of the cycle time later than the previous step so that there are two beds on adsorption all the time. In addition, two beds are under regeneration at any given time.

[0046] Given the fact that the mass transfer layer has certain length, it is still desirable to have more beds on feed if doing so does not cause a large negative impact on performance by reducing the time for other steps. Notice that in the process whose cycle chart is shown in Table 2, 1/20 of the cycle time is idle, meaning that the bed is not used in that 5% of the cycle time. That idle time can be used for adsorption by shifting it to the adsorption step. In order to

EP 1 118 370 A1

maintain synchronization of the beds providing gas for pressure equalization and those receiving gas for pressure equalization, and to have three beds on adsorption all the time, one more of these 1/20 cycle slots has to be allocated to adsorption. This can be accomplished by eliminating the fourth step of providing gas for pressure equalization, and providing the gas for the fourth step of pressure equalization from the bed that is providing gas for purge at that time, as shown in the following table:

TABLE 3

	A	A	A	A	A	A	1	2	3	P'	P	B	B	G	G	4'	3'	2'	1'	R
10	1'	R	A	A	A	A	A	A	1	2	3	P'	P	B	B	G	G	4'	3'	2'
	3'	2'	1'	R	A	A	A	A	A	1	2	3	P'	P	B	B	G	G	4'	
	G	4'	3'	2'	1'	R	A	A	A	A	A	1	2	3	P'	P	B	B	G	
15	B	G	G	4'	3'	2'	1'	R	A	A	A	A	A	1	2	3	P'	P	B	
	P	B	B	G	G	4'	3'	2'	1'	R	A	A	A	A	A	1	2	3	P'	
	3	P'	P	B	B	G	G	4'	3'	2'	1'	R	A	A	A	A	A	1	2	
	1	2	3	P'	P	B	B	G	G	4'	3'	2'	1'	R	A	A	A	A	A	
20	A	A	1	2	3	P'	P	B	B	G	G	4'	3'	2'	1'	R	A	A	A	
	A	A	A	A	1	2	3	P'	P	B	B	G	G	4'	3'	2'	1'	R	A	

[0047] In this cycle, in the first 1/20 of the cycle time of the provide purge step (indicated by "P' "s), the provide purge bed simultaneously provides gas to the bed in its purge step (indicated by "G"s) and to the bed on the receiving end of the fourth step of pressure equalization (indicated by "4'"). The rest is kept as in the cycle shown in Table 2.

[0048] In yet another embodiment, two beds are always on adsorption. After the completion of the adsorption step, the bed goes through four steps of pressure equalization on the provide gas side. Then the bed provides gas for purge for 3/20 of the cycle time, followed by 1/20 of the cycle time for blowdown, 3/20 of the cycle time for purge, 4 steps of pressure equalization on the receiving gas end, and 1/20 of the cycle time for re-pressurization, as shown in the following table:

TABLE 4

	A	A	A	A	1	2	3	4	P	P	P	B	G	G	G	4'	3'	2'	1'	R
35	1'	R	A	A	A	A	1	2	3	4	P	P	P	B	G	G	G	4'	3'	2'
	3'	2'	1'	R	A	A	A	A	1	2	3	4	P	P	P	B	G	G	G	4'
	G	4'	3'	2'	1'	R	A	A	A	A	1	2	3	4	P	P	P	B	G	G
40	G	G	G	4'	3'	2'	1'	R	A	A	A	A	1	2	3	4	P	P	P	B
	P	B	G	G	G	4'	3'	2'	1'	R	A	A	A	A	1	2	3	4	P	P
	P	P	P	B	G	G	G	4'	3'	2'	1'	R	A	A	A	A	1	2	3	4
	3	4	P	P	P	B	G	G	G	4'	3'	2'	1'	R	A	A	A	A	1	2
45	1	2	3	4	P	P	P	B	G	G	G	4'	3'	2'	1'	R	A	A	A	A
	A	A	1	2	3	4	P	P	P	B	G	G	G	4'	3'	2'	1'	R	A	A

[0049] Tables 2-4 show the first embodiment of the invention, wherein the PSA system employs ten adsorbent beds and four steps of equalization. Table 5, below, shows a cycle chart for a process in accordance with the first and second embodiments of the invention. That is, in addition to having ten adsorbent beds and four steps of equalization, the process of Table 5 has at least two beds being counter-currently purged at any given time.

[0050] Increasing the purge time can improve the adsorption capacity and increase recovery simultaneously. Increasing the purge time also increases the provide purge time following the conventional ways of constructing cycles. In the following embodiment, one provide purge bed provides the purge gas for two beds:

EP 1 118 370 A1

TABLE 5

	A	A	A	A	1	2	3	P'	P	B	B	G	G	G	G	4'	3'	2'	1'	R
5	1'	R	A	A	A	A	1	2	3	P'	P	B	B	G	G	G	G	4'	3'	2'
	3'	2'	1'	R	A	A	A	A	1	2	3	P'	P	B	B	G	G	G	G	4'
	G	4'	3'	2'	1'	R	A	A	A	A	1	2	3	P'	P	B	B	G	G	G
	G	G	G	4'	3'	2'	1'	R	A	A	A	A	1	2	3	P'	P	B	B	G
10	B	G	G	G	G	4'	3'	2'	1'	R	A	A	A	A	1	2	3	P'	P	B
	P	B	B	G	G	G	G	4'	3'	2'	1'	R	A	A	A	A	1	2	3	P'
	3	P'	P	B	B	G	G	G	G	4'	3'	2'	1'	R	A	A	A	A	1	2
15	1	2	3	P'	P	B	B	G	G	G	G	4'	3'	2'	1'	R	A	A	A	A
	A	A	1	2	3	P'	P	B	B	G	G	G	G	4'	3'	2'	1'	R	A	A

In addition, this bed is also used to provide the gas for the fourth step of pressure equalization during the first half of the provide purge step (P'). This enables doubling the purge time, and at the same time employing four steps of pressure equalization for a ten-bed system with two beds on adsorption.

[0051] The second embodiment of the invention is not limited to ten-bed devices or four equalization steps, as in the process depicted in Table 5.

[0052] For example, a 12 bed cycle with double purge time, 4 steps of pressure equalization and 3 beds on adsorption is shown in the following table:

9

EP 1 118 370 A1

[0053] In the process shown in Table 6, the highest pressure equalization step is separate from the product re-pressurization step. The bed providing purge gas provides purge gas to two beds. In the first half of the providing purge gas step (P'), this bed also provides gas to the lowest pressure step of pressure equalization.

[0054] A 12 bed cycle with double purge time, 4 steps of pressure equalization and 4 beds on adsorption is shown in the following table:

5

10

15

20

25

30

35

40

45

50

55

11

EP 1 118 370 A1

[0055] In the process shown in Table 7, the bed providing purge gas provides purge gas to two beds. In the first half of the providing purge gas step, this bed also provides gas to the lowest pressure step of pressure equalization.

[0056] A 12 bed cycle with triple purge time, 4 steps of pressure equalization and 3 beds on adsorption is shown in the following table:

5

10

15

20

25

30

35

40

45

50

55

13

EP 1 118 370 A1

[0057] In the process shown in Table 8, the bed providing purge gas provides purge gas to three beds. In the first half of the providing purge gas step (P'), this bed also provides gas to the lowest pressure step of pressure equalization.

[0058] Tables 5-8 are illustrative and not limiting. For example, the increased purge time embodiment of the invention encompasses the use of any number of beds, although 10-12 beds are preferred, and encompasses cycles with less or more than four steps of pressure equalization.

[0059] The invention will be illustrated in more detail with reference to the following Examples, but it should be understood that the present invention is not deemed to be limited thereto.

Example 1

[0060] The unexpected advantages of the invention are demonstrated by the following simulation comparing a ten-bed embodiment of the invention (see Table 2, above) with a twelve-bed cycle in accordance with the prior art (see Table 1, above).

[0061] The pressure and temperature specified in the simulations were 30 atmospheres and 100°F, respectively. The composition specified in the simulations contained 0.5% nitrogen, 6% methane, 16% carbon dioxide, 3.5% carbon monoxide and 74% hydrogen. The key operating parameters and results are summarized in Table 9:

TABLE 9

Cycle	Table 1 (Comparative)	Table 2 (Invention)
Bed diameter (ft)	11.0	11.5
Bed length (ft)	22.4	22.4
Feed time (s)	240	128
Production (million scf/d)	84.2	83.5
Recovery	88.2%	88.0%
CO in product (ppm)	1.0	1.0
N ₂ in product (ppm)	620	332

[0062] It can be seen from Table 9 that the recoveries of the two cycles are virtually the same. The N₂ content is much lower with the ten-bed cycle according to the invention. The amount of adsorbent needed for a certain production rate is reduced by 9%, and the number of beds is reduced from 12 to 10. That not only means that the costs of vessels and skids are reduced, it also means that the costs of valves and connecting pipes connecting these beds are reduced as the consequence of bed reduction.

Example 2

[0063] The efficacy of increasing the purge time in accordance with the invention can be demonstrated by comparing the simulation results of the process of Table 1 (i.e., a 12 bed cycle with 4 beds on adsorption and 4 steps of pressure equalization) with those of Table 5 (i.e., a 10 bed cycle with 4 steps of pressure equalization, double purge time, and 2 beds on adsorption). The pressure and temperature specified in the simulations were 30 atmospheres and 100°F, respectively. The composition specified in the simulations contained 0.5% nitrogen, 6% methane, 16% carbon dioxide, 3.5% carbon monoxide and 74% hydrogen. Each bed has two sections: (1) a section closer to the feed nozzle, with 50% of the bed length, containing carbon adsorbent; and (2) a section further from the feed nozzle containing a zeolite adsorbent. The key operating parameters and results are summarized in Table 10:

TABLE 10

Cycle	Table 1 (Comparative)	Table 5 (Invention)
Bed Diameter (ft)	11.0	11.0
Bed length (ft)	22.4	22.4
Hydrogen Production (million scf/d)	84.2	79.9
Hydrogen Recovery	88.2	89.21
CO in product (ppm)	1.0	0.2

EP 1 118 370 A1

TABLE 10 (continued)

Cycle	Table 1 (Comparative)	Table 5 (Invention)
Nitrogen in product (ppm)	620	1005

[0064] It can be seen from Table 10 that using the cycle in Table 5, it is possible to eliminate two beds and the associated valves, piping and adsorbents, and at the same time increase hydrogen recovery by 1%. Moreover, the diameters of the beds in this cycle are smaller. The total amount of adsorbent is reduced by 36%. If the bed diameters were equal, the hydrogen production would be greater for the cycle in Table 5 with a similar recovery benefit. The modifications that may be needed to achieve these are (1) arranging piping and valves such that one provide purge bed can provide gas to three beds with the desired flows, and (2) arranging pipes and valves such that off-gas can be collected from one blowdown bed and two purge beds. One way of doing so is to use a valve with a positioner on the off-gas line of each bed so that the off-gas flow from each individual bed can be independently controlled.

[0065] While the invention has been described in detail and with reference to specific examples thereof, it will be apparent to one skilled in the art that various changes and modifications can be made therein without departing from the spirit and scope thereof.

Claims

1. A pressure swing adsorption process comprising providing a pressure swing adsorption apparatus having ten beds, and equalizing a pressure of each of said ten beds in four steps.
2. The process of claim 1, wherein at all times during said process, an average of at least two of said ten beds are being simultaneously regenerated by simultaneously providing off-gas from a feed end of each of said two beds to an off-gas line.
3. The process of claim 1, wherein each of said four steps comprises a depressurizing provide equalization phase spanning about 1/20 of a total cycle time of said process and a repressurization phase "R" spanning about 1/20 of said total cycle time.
4. The process of claim 1, wherein hydrogen is a product of said process.
5. The process of claim 1, represented by the following cycle chart:

A	A	A	A	1	2	3	4	P	P	B	B	G	G	I	4'	3'	2'	1'	R
1'	R	A	A	A	A	1	2	3	4	P	P	B	B	G	G	I	4'	3'	2'
3'	2'	1'	R	A	A	A	A	1	2	3	4	P	P	B	B	G	G	I	4'
I	4'	3'	2'	1'	R	A	A	A	A	1	2	3	4	P	P	B	B	G	G
G	G	I	4'	3'	2'	1'	R	A	A	A	A	1	2	3	4	P	P	B	B
B	B	G	G	I	4'	3'	2'	1'	R	A	A	A	A	1	2	3	4	P	P
P	P	B	B	G	G	I	4'	3'	2'	1'	R	A	A	A	A	1	2	3	4
3	4	P	P	B	B	G	G	I	4'	3'	2'	1'	R	A	A	A	A	1	2
1	2	3	4	P	P	B	B	G	G	I	4'	3'	2'	1'	R	A	A	A	A
A	A	1	2	3	4	P	P	B	B	G	G	I	4'	3'	2'	1'	R	A	A

wherein A is adsorption, 1 is providing gas for a first step of pressure equalization, 2 is providing gas for a second step of pressure equalization, 3 is providing gas for a third step of pressure equalization, 4 is providing gas for a fourth step of pressure equalization, P is providing purge gas, B is counter-current blowdown, G is counter-current purge, I is idle, 4' is receiving gas for the fourth step of pressure equalization, 3' is receiving gas for the third step of pressure equalization, 2' is receiving gas for the second step of pressure equalization, and 1' is receiving gas for the first step of pressure equalization and simultaneously receiving product gas for repressurization, and R is repressurizing with product gas.

EP 1 118 370 A1

6. The process of claim 1, represented by the following cycle chart:

	A	A	A	A	A	1	2	3	P'	P	B	B	G	G	4'	3'	2'	1'	R
5	1'	R	A	A	A	A	A	1	2	3	P'	P	B	B	G	G	4'	3'	2'
	3'	2'	1'	R	A	A	A	A	A	1	2	3	P'	P	B	B	G	G	4'
	G	4'	3'	2'	1'	R	A	A	A	A	A	1	2	3	P'	P	B	B	G
	B	G	G	4'	3'	2'	1'	R	A	A	A	A	A	1	2	3	P'	P	B
10	P	B	B	G	G	4'	3'	2'	1'	R	A	A	A	A	A	1	2	3	P'
	3	P'	P	B	B	G	G	4'	3'	2'	1'	R	A	A	A	A	A	1	2
	1	2	3	P'	P	B	B	G	G	4'	3'	2'	1'	R	A	A	A	A	A
15	A	A	1	2	3	P'	P	B	B	G	G	4'	3'	2'	1'	R	A	A	A
	A	A	A	A	1	2	3	P'	P	B	B	G	G	4'	3'	2'	1'	R	A

wherein A is adsorption, 1 is providing gas for a first step of pressure equalization, 2 is providing gas for a second step of pressure equalization, 3 is providing gas for a third step of pressure equalization, P' is providing purge gas and simultaneously providing gas for a fourth step of pressure equalization, P is providing purge gas, B is counter-current blowdown, G is counter-current purge, I is idle, 4' is receiving gas for the fourth step of pressure equalization, 3' is receiving gas for the third step of pressure equalization, 2' is receiving gas for the second step of pressure equalization, and 1' is receiving gas for the first step of pressure equalization and simultaneously receiving product gas for repressurization, and R is repressurizing with product gas.

7. The process of claim 1, represented by the following cycle chart:

	A	A	A	A	1	2	3	4	P	P	P	B	G	G	G	4'	3'	2'	1'	R
30	1'	R	A	A	A	A	1	2	3	4	P	P	P	B	G	G	G	4'	3'	2'
	3'	2'	1'	R	A	A	A	A	1	2	3	4	P	P	P	B	G	G	G	4'
	G	4'	3'	2'	1'	R	A	A	A	A	1	2	3	4	P	P	P	B	G	G
35	G	G	G	4'	3'	2'	1'	R	A	A	A	A	1	2	3	4	P	P	P	B
	P	B	G	G	G	4'	3'	2'	1'	R	A	A	A	A	1	2	3	4	P	P
	P	P	P	B	G	G	G	4'	3'	2'	1'	R	A	A	A	A	1	2	3	4
	3	4	P	P	P	B	G	G	G	4'	3'	2'	1'	R	A	A	A	A	1	2
40	1	2	3	4	P	P	P	B	G	G	G	4'	3'	2'	1'	R	A	A	A	A
	A	A	1	2	3	4	P	P	P	B	G	G	G	4'	3'	2'	1'	R	A	A

wherein A is adsorption, 1 is a first step of pressure equalization, 2 is a second step of pressure equalization, 3 is a third step of pressure equalization, 4 is a fourth step of pressure equalization, P is purge, B is counter-current blowdown, G is counter-current purge, I is idle, 4' is receive gas for the fourth step of pressure equalization, 3' is receive gas for the third step of pressure equalization, 2' is receive gas for the second step of pressure equalization, and 1' is receive gas for the first step of pressure equalization and simultaneously receive product gas for repressurization, and R is bed repressurizing with product gas.

8. The process of claim 1, wherein at all times during said process, an average of at least two of said ten beds are being counter-currently purged.

9. The process of claim 8, represented by the following cycle chart:

55	A	A	A	A	1	2	3	P'	P	B	B	G	G	G	G	4'	3'	2'	1'	R
	1'	R	A	A	A	A	1	2	3	P'	P	B	B	G	G	G	G	4'	3'	2'

EP 1 118 370 A1

(continued)

	3'	2'	1'	R	A	A	A	A	1	2	3	P'	P	B	B	G	G	G	G	4'
5	G	4'	3'	2'	1'	R	A	A	A	A	1	2	3	P'	P	B	B	G	G	G
	G	G	G	4'	3'	2'	1'	R	A	A	A	A	1	2	3	P'	P	B	B	G
	B	G	G	G	G	4'	3'	2'	1'	R	A	A	A	A	1	2	3	P'	P	B
	P	B	B	G	G	G	G	4'	3'	2'	1'	R	A	A	A	A	1	2	3	P'
10	3	P'	P	B	B	G	G	G	G	4'	3'	2'	1'	R	A	A	A	A	1	2
	1	2	3	P'	P	B	B	G	G	G	G	4'	3'	2'	1'	R	A	A	A	A
	A	A	1	2	3	P'	P	B	B	G	G	G	G	4'	3'	2'	1'	R	A	A

15 wherein A is adsorption, 1 is providing gas for a first step of pressure equalization, 2 is providing gas for a second step of pressure equalization, 3 is providing gas for a third step of pressure equalization, P' is providing purge gas and simultaneously providing gas for a fourth step of pressure equalization, P is providing purge gas, B is counter-current blowdown, G is counter-current purge, I is idle, 4' is receiving gas for the fourth step of pressure equalization, 3' is receiving gas for the third step of pressure equalization, 2' is receiving gas for the second step of pressure
 20 equalization, and 1' is receiving gas for the first step of pressure equalization and simultaneously receiving product gas for repressurization, and R is repressurizing with product gas.

10. A pressure swing adsorption process comprising:

- 25 (a) providing an adsorption apparatus having a plurality of beds;
 (b) at least one adsorption step comprising feeding a feed mixture to a feed end of a first bed, adsorbing impurities onto an adsorbent in said first bed and permitting a product gas to exit a product end of said first bed;
 (c) at least one depressurizing equalization step comprising reducing a pressure in said first bed by closing a feed valve and sequentially releasing gas from a product end of said first bed to other beds or to at least one
 30 other bed and a tank;
 (d) at least one pressure reduction step comprising further reducing said pressure of said first bed co-currently and/or counter-currently;
 (e) at least one counter-current purging step, comprising counter-currently purging said first bed with gas from another bed for a duration such that at least two of said beds of said apparatus are being purged simultaneously
 35 throughout said process;
 (f) at least one repressurizing equalization step comprising increasing the pressure of said first bed with gas released from at least one other bed and/or tank undergoing said pressure reducing step; and
 (g) at least one pressure augmentation step comprising further increasing said pressure of said first bed by feeding to said first bed at least one of a counter-current stream of product gas and a co-current stream of
 40 feed gas.

11. The process of claim 10, wherein said apparatus has ten beds and four pressure equalizations per bed are performed throughout said process.

45 12. The process of claim 10, wherein said product gas is hydrogen.

13. The process of claim 10, wherein said feed mixture comprises hydrogen and at least one member selected from the group consisting of methane, carbon dioxide, carbon monoxide, nitrogen and water vapor.

50 14. The process of claim 13, wherein said feed gas is obtained by steam reforming of hydrocarbons.

15. The process of claim 13, wherein said feed gas is obtained by partial oxidation of hydrocarbons.

55 16. The process of claim 15, wherein said partial oxidation occurs in a presence of at least one catalyst.

17. The process of claim 15, wherein oxygen used in said partial oxidation is provided by an ion transport membrane.

EP 1 118 370 A1

18. The process of claim 17, wherein said ion transport membrane is integrated with a reactor in which said partial oxidation occurs.
19. The process of claim 10, wherein said steps are sequential.
20. The process of claim 10, wherein at least a part of said at least one repressurizing equalization step overlaps in time with said at least one pressure augmentation step.
21. The process of claim 10, wherein at least a part of said at least one repressurizing equalization step overlaps in time with at least one of counter-current repressurization by the product gas and co-current repressurization by the feed gas.
22. The process of claim 10, wherein gas from the product end of the bed in said at least one depressurizing equalization step is transferred directly to a bed in said at least one repressurizing equalization step.
23. The process of claim 10, wherein gas from the product end of the bed in said at least one depressurizing equalization step is transferred to a tank before being transferred to a bed in said at least one repressurizing equalization step.
24. The process of claim 10, wherein a bed being co-currently depressurized according to said at least one pressure reduction step provides purge gas to more than one other bed.
25. The process of claim 24, wherein said depressurizing equalization step precedes said provide purge step.
26. The process of claim 24, wherein said depressurizing equalization step overlaps in time with at least some portion of said provide purge step.
27. The process of claim 24, wherein said depressurizing equalization step follows said provide purge step.
28. The process of claim 10, wherein a bed being co-currently depressurized according to said at least one pressure reduction step provides gas for pressure equalization of at least one other bed, as well as purge gas to more than one other bed.
29. The process of claim 10, represented by the following cycle chart:

19

EP 1 118 370 A1

wherein A is adsorption, 1 is providing gas for a first step of pressure equalization, 2 is providing gas for a second step of pressure equalization, 3 is providing gas for a third step of pressure equalization, P' is providing purge gas and simultaneously providing gas for a fourth step of pressure equalization, P is providing purge gas, B is counter-current blowdown, G is counter-current purge, I is idle, 4' is receiving gas for the fourth step of pressure equalization, 3' is receiving gas for the third step of pressure equalization, 2' is receiving gas for the second step of pressure equalization, and 1' is receiving gas for the first step of pressure equalization and simultaneously receiving product gas for re-pressurization, and R is repressurizing with product gas.

30. The process of claim 10, represented by the following cycle chart:

21

EP 1 118 370 A1

wherein A is adsorption, 1 is providing gas for a first step of pressure equalization, 2 is providing gas for a second step of pressure equalization, 3 is providing gas for a third step of pressure equalization, 4 is providing gas for a fourth step of pressure equalization, P is providing purge gas, B is counter-current blowdown, G is counter-current purge, I is idle, 4' is receiving gas for the fourth step of pressure equalization, 3' is receiving gas for the third step of pressure equalization, 2' is receiving gas for the second step of pressure equalization, and 1' is receiving gas for the first step of pressure equalization and simultaneously receiving product gas for re-pressurization, and R is repressurizing with product gas.

31. The process of claim 10, represented by the following cycle chart:

10

15

20

25

30

35

40

45

50

55

23

EP 1 118 370 A1

wherein A is adsorption, 1 is providing gas for a first step of pressure equalization, 2 is providing gas for a second step of pressure equalization, 3 is providing gas for a third step of pressure equalization, P' is providing purge gas and simultaneously providing gas for a fourth step of pressure equalization, P is providing purge gas, B is counter-current blowdown, G is counter-current purge, I is idle, 4' is receiving gas for the fourth step of pressure equalization, 3' is receiving gas for the third step of pressure equalization, 2' is receiving gas for the second step of pressure equalization, and 1' is receiving gas for the first step of pressure equalization and simultaneously receiving product gas for re-pressurization, and R is repressurizing with product gas.

5

10

15

20

25

30

35

40

45

50

55

EP 1 118 370 A1

European Patent
Office

EUROPEAN SEARCH REPORT

Application Number
EP 01 10 0128

DOCUMENTS CONSIDERED TO BE RELEVANT			
Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	CLASSIFICATION OF THE APPLICATION (Int.Cl.7)
X	US 4 375 363 A (A. FUDERER) 1 March 1983 (1983-03-01) * the whole document *	1-31	B01D53/047 C01B3/02
X	US 4 475 929 A (A. FUDERER) 9 October 1984 (1984-10-09) * the whole document *	1-31	
X	DE 30 32 799 A (UNION CARBIDE) 25 March 1982 (1982-03-25) * the whole document *	1-31	
D, X	US 3 986 849 A (A. FUDERER) 19 October 1976 (1976-10-19) * the whole document *	1-31	
			TECHNICAL FIELDS SEARCHED (Int.Cl.7)
			B01D C01B
The present search report has been drawn up for all claims			
Place of search THE HAGUE		Date of completion of the search 26 April 2001	Examiner Bogaerts, M
CATEGORY OF CITED DOCUMENTS X : particularly relevant if taken alone Y : particularly relevant if combined with another document of the same category A : technological background O : non-written disclosure P : intermediate document T : theory or principle underlying the invention E : earlier patent document, but published on, or after the filing date D : document cited in the application L : document cited for other reasons & : member of the same patent family, corresponding document			

EPO FORM 1503 03 82 (P0401)

EP 1 118 370 A1

ANNEX TO THE EUROPEAN SEARCH REPORT
ON EUROPEAN PATENT APPLICATION NO.

EP 01 10 0128

This annex lists the patent family members relating to the patent documents cited in the above-mentioned European search report. The members are as contained in the European Patent Office EDP file on
The European Patent Office is in no way liable for these particulars which are merely given for the purpose of information.

26-04-2001

Patent document cited in search report	Publication date	Patent family member(s)	Publication date
US 4375363 A	01-03-1983	US 4475929 A	09-10-1984
US 4475929 A	09-10-1984	US 4375363 A	01-03-1983
DE 3032799 A	25-03-1982	BE 885126 A	09-03-1981
US 3986849 A	19-10-1976	AR 216443 A	28-12-1979
		AU 497183 B	07-12-1978
		AU 1544476 A	05-01-1978
		BE 843656 A	30-12-1976
		BR 7604261 A	26-07-1977
		CA 1076967 A	06-05-1980
		DD 129292 A	11-01-1978
		DE 2629450 A	12-05-1977
		EG 12468 A	30-06-1979
		ES 449343 A	01-12-1977
		FR 2330433 A	03-06-1977
		GB 1505957 A	05-04-1978
		IL 49941 A	31-01-1979
		IN 145501 A	28-10-1978
		IT 1062023 B	25-06-1983
		JP 1110050 C	31-08-1982
		JP 52059073 A	16-05-1977
		JP 57002046 B	13-01-1982
		MX 143326 A	15-04-1981
		MY 1581 A	31-12-1981
		NL 7607199 A, B,	10-05-1977
		NO 762269 A, B,	10-05-1977
		SE 422743 B	29-03-1982
		SE 7607460 A	08-05-1977
		TR 19004 A	22-02-1978
		YU 160076 A	31-05-1982
		ZA 7603104 A	25-05-1977

EPO FORM P-489

For more details about this annex : see Official Journal of the European Patent Office, No. 12/82